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By conducting a series of experiments, it was discovered that process parameters had an impact on the strength and hardness of the AA 2024/TiC/E-Glass alloy.

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ABSTRACT

The aerospace industry's demand for engineering materials is growing by the day. Specific applications for AA 2024 alloy with titanium carbide particles and E-Glass fibre include aircraft structure, window panel, seats, aircraft fittings, and wheels. As a result, in this study, Al 2024 alloy was chosen as the matrix, with titanium carbide particles and E-Glass fibre as reinforcement. Titanium carbide particles with an average size of 40 micrometres, E-Glass fibre were chosen and incorporated in varying weight percentages into the Al 2024 matrix via the stir casting process. To validate the experimental values, Taguchi's Technique was used to evaluate optimization, the influence of process parameters, and the regression equation. Tensile strength and hardness were found to enhance as the weight percentage of titanium carbide particles and E-Glass in the Al 2024 alloy increased. SEM images reveal that titanium carbide particles E-Glass are uniformly distributed in the Al 2024 alloy, and dimple structures form at the tensile fracture surface.

KEYWORDS:Titanium carbide particles, E-Glass, Al 2024 alloy composite, tensile strength and hardness

1. INTRODUCTION

Extensive materials research has resulted in a plethora of new scientific innovations aimed at synthesising special materials with increased efficiency and low manufacturing costs in order to meet the engineering sector's long-standing demands. A novel material system containing hard particulates embedded in a metal matrix demonstrated superior operating performance and enhanced tribological properties [1], [2].

Among MMCs, aluminium alloy-based composites demonstrated significant improvements in mechanical, thermal, electrical, and wear properties to meet industry demands. Due to their superior machining, joining, and processability, aluminium alloys are referred to as versatile materials that can be used in a wide variety of engineering applications. Additionally, Al alloys' low cost, increased strength-to-weight ratio, and other environmentally friendly properties make them a preferred material for engineering applications [3], [4].

Among the aluminium alloys, Al-Si is a well-known casting alloy due to its high wear resistance, low thermal expansion coefficient, excellent corrosion resistance, and improved mechanical properties over a wide temperature range. The grain refiner elements convert the coarse Si morphology to lamellar (fine) Si, thereby improving the mechanical properties [5].

Diverse researchers developed a variety of composite materials by varying the matrix, reinforcement size, shape, and volume, as well as the processing technique, to meet the requirements and applications. To optimise the properties of the metal matrix composite, the second phase's distribution within the matrix alloy must be uniform, and the wettability or bonding between these substances must be optimised. [6].

2. METHODOLOGY

2.1 Die Casting:

Is a method of metal casting that involves forcing molten metal into a mould cavity under high pressure [7]. The majority of die castings are made of non-ferrous metals, most notably zinc, copper, aluminium, magnesium, lead, pewter, and tin alloys. Lubricant is sprayed into the cavity of the dies to prepare them. Lubricant assists in regulating the die's temperature and also aids in the casting's removal. The dies are then sealed and molten metal is injected into them at high pressures ranging from 10 to 175 MPa (1,500 and 25,400 psi). After filling the mould cavity, pressure is maintained until the casting solidifies.

2.2 Machining:

Because the casted specimens will not have the required dimensions [8], they are further machined into the desired shape using a lathe in the machine shop. The specimen's centre portion diameter should be consistent with the standard before it is tested on the machine.

2.3 Design of Experiments:

Design of Experiments (DoE) is used to know the response of an output variable with the effect of input factors at the same time. Determining changes are made in the input factor for the series of experimental runs. The information has been gathered for each run. Standard experiment layout having 2 factors with 4 levels each, for L16 (24) Orthogonal Array (OA) was adopted by using Taguchi's Technique. Table 1 shows the L16 (24) Taguchi orthogonal array table. The experimental values of tensile strength and hardness of the formed composites under various parameters are tabulated in Table 2.

Table 1 Taguchi Orthogonal Array Table

Run #	Taguchi P = TiC	E-Glass	Х
Kun #			λ
	(Weight percent)	(Weight percent)	
1	0	0	X_1
2	0	1	χ_2
3	0	3	Х3
4	0	5	X_1
5	2	0	χ_5
6	2	1	χ_6
7	2 /	3	χ_7
8	2	5	χ_8
9	4	0	χ_9
10	4	1	X_{10}
11	4	3	X_{11}
12	4	5	X_{12}
13	6	0	X_{13}
14	6	1	X_{14}
15	6	3	X_{15}
16	6	5	X_{16}

Table 2 Taguchi Orthogonal Array Table

		Taguchi P = 2, L = 4		
Run	TiC	E-Glass	<mark>Ultim</mark> ate	Hardness
#	(Weight	(Weight	Tensile	(BHN)
	percent)	percent)	Strength	-
			(MPa)	
1	0	0	153.384	46.2
2	0	1	160.839	48.3
3	0	3	171.169	49.9
4	0	5	188.832	56.2
5	2	0	164.868	49.2
6	2	1	183.245	54.7
7	2	3	188.576	56.8
8	2	5	191.719	60.1
9	4	0	181.937	55.3
10	4	1	209.824	63.2
11	4	3	216.805	65.5
12	4	5	231.485	69.1
13	6	0	187.708	57.4
14	6		216.132	65.1
15	6	3	233.686	70.6
16	6	9 5	240.759	72.3

3. RESULTS AND DISCUSSION

Figure 1 and 2 (a-c) shows the influence of TiC and E-Glass on Al 2024 related to ultimate tensile strength and hardness for the Al 2024 / TiC / E-Glass composite. It is noticed that for the factors 6 weight percent TiC and 5 $\,$

weight percent of E-Glass have a better significant value on both ultimate tensile strength and hardness.

Tables 3 and 4 shows the response table for ultimate tensile strength and hardness for means for the factor (weight percent of TiC and E-Glass on Al 2024 alloy.

With the help of ANOVA analysis (ref table 5 and 6), the effect of process parameters on ultimate tensile strength and hardness on Al 2024 alloy are also discussed. Expected values for tensile strength and hardness were calculated using regression equations and tabulated in table 7. Within the factors, the regression equation is used to project the ultimate tensile strength and hardness.

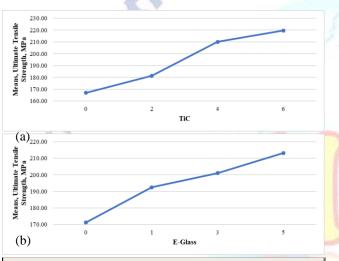
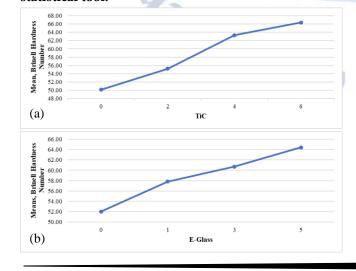




Figure 1 Effect of individual parameters on ultimate tensile strength value of Al 2024 / TiC / E-Glass (a) TiC, (b) E-Glass, and (c) graph obtained from mini stab statistical tool.



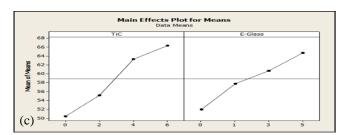


Figure 2 Effect of individual parameters on Brinell hardness number value of Al 2024 / TiC / E-Glass (a) TiC, (b) E-Glass, and (c) graph obtained from mini stab statistical tool.

The regression equations for tensile strength and hardness are:

Ultimate Tensile Strength = 149.605 + 9.31033 * TiC + 7.5389 * E-Glass (Eqn 1)

BHN = 45.2384 + 2.78875 * TiC + 2.31737 * E-Glass (Eqn 2)

Table 3 Response table - ultimate tensile strength of Al 2024 / TiC / E-Glass for Means

Level	TiC	E-Glass		
1	167.1	171.2		
2	181.4	192.5		
3	210.0	201.1		
4	219.6	213.2		
Delta	52.5	42		
Rank	1	2		

Table 4 Response table – Brinell Hardness of Al 2024 /
TiC / E-Glass for Means

Level	TiC	E-Glass
1	167.1	171.2
2	181.4	192.5
3	210.0	201.1
4	219.6	213.2
Delta	52.5	42
Rank	1	2

Table 5 Results of ANOVA on ultimate tensile strength of Al 2024 / TiC / E-Glass obtained from mini tab

statistical tool				
Source	TiC	E-Glass	Error	Total
DF	3	3	9	15
Seq SS	7181	3753.5	463.4	11397.9
Adj SS	7181	3753.5	463.4	
Adj MS	2393.7	1251.2	51.5	
F-Value	46.49	24.3		
P-Value	0	0		
% of Contribution	63.00%	32.93%	4.07%	
Rank	1	2		

Table 6 Results of ANOVA on Brinell hardness number of Al 2024 / TiC / E-Glass obtained from mini tab statistical tool

Source	TiC	E-Glass	Error	Total
DF	3	3	9	15
Seq SS	638.84	342.26	29.47	1010.56
Adj SS	638.84	342.26	29.47	
Adj MS	212.95	114.09	3.27	
F-Value	65.04	34.85		10
P-Value	0	0	4	-+ 0
% of Contribution	63.22%	33.87%	2.92%	
DF	3	3	9	15

Table 7 Comparison of experimental results - ultimate tensile strength, Brinell hardness number v/s regression equation of Al 2024 / TiC / E-Glass

Tensile (M			Error	Brinell Hardness Number		Error
Run #	Experi mental	Reg. Eq. 1	%	Experi mental	Reg. Eq. 1	%
1	153.384	149.605	2.46%	46.200	45.238	2.08%
2	160.839	157.144	2.30%	48.300	47.556	1.54%
3	171.169	172.222	0.62%	<mark>49.90</mark> 0	52.191	4.59%
4	188.832	187.300	0.81%	<mark>56.20</mark> 0	56.825	1.11%
5	164.868	168.226	2.04%	49.200	50.816	3.28%
6	183.245	175.765	4.08%	54.700	53.133	2.86%
7	188.576	190.842	1.20%	56.800	57.768	1.70%
8	191.719	205.920	7.41%	60.100	62.403	3.83%
9	181.937	186.846	2.70%	55.300	56.393	1.98%
10	209.824	194.385	7.36%	63.200	58.711	7.10%
11	216.805	209.463	3.39%	65.500	63.346	3.29%
12	231.485	224.541	3.00%	69.100	67.980	1.62%
13	187.708	205.467	9.46%	57.400	61.971	7.96%
14	216.132	213.006	1.45%	65.100	64.288	1.25%
15	233.686	228.084	2.40%	70.600	68.923	2.38%
16	240.759	243.161	1.00%	72.300	73.558	1.74%

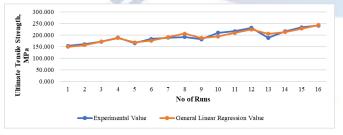


Figure 3 ultimate tensile strength experimental value v/s general linear regression value of Al 2024 / TiC / E-Glass

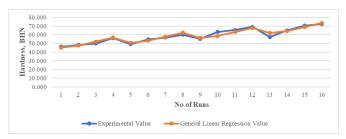


Figure 4 Brinell hardness number experimental value v/s general linear regression value of Al 2024 / TiC / E-Glass

Table 8 Summary of the Model for Ultimate Tensile Strength - Al 2024 / TiC / E-Glass

S	R-Sq	R-Sq(adj)
7.17542	95.93%	93.22%

Table 9 Summary of the Model for Brinell Hardness Number - Al 2024 / TiC / E-Glass

S	R-Sq	R-Sq(adj)
1.80941	97.08%	95.14%

Figure 3 and 4 reveals the confirmation of the experimental values with the expected values. The stable experimentations have been conducted at confidence intervals of 95% and the comparison of experimental values Vs. expected values have been observed with two factors at four levels each. Experimental values are slight variations with the expected values for both the ultimate tensile strength and hardness of the composite material and hence the experimental values are validated.

The summary of the model for tensile strength and hardness on Al 2024 alloy by ANOVA technique is shown in Tables 5 and 6.

Table 5 and 6 it is revealed that the percentage contribution for ultimate tensile strength is highest for the TiC particles is 63.00 % whereas E-Glass is 32.93 %, hence TiC has a more significant impact on ultimate tensile strength when compared to the other factor. While percentage contribution for hardness is highest for the TiC is 66.00 % whereas E-Glass is 33.87 %, hence TiC has a more significant impact on hardness when compared to the other factor.

4.CONCLUSION

Al 2024 / TiC / E-Glass composite can be successfully synthesized through the stir casting technique. The optimum parameter is 6 weight percent TiC and 5 weight

percent E-Glass found to be enhanced by 56.96 percent ultimate tensile strength and hardness by 56.49 percent.

Conflict of interest statement

Authors declare that they do not have any conflict of interest.

REFERENCES

- [1] A. N. Abdel-Azim, Y. Shash, S. F. Mostafa, and A. Younan, "Casting of 2024-Al alloy reinforced with Al2O3 particles," Journal of Materials Processing Tech., vol. 55, no. 3–4, pp. 199–205, 1995, doi: 10.1016/0924-0136(95)01954-5.
- [2] A. Albiter, A. Contreras, E. Bedolla, and R. Perez, "Structural and chemical characterization of precipitates in Al-2024/TiC composites," Composites Part A: Applied Science and Manufacturing, vol. 34, no. 1, pp. 17–24, 2003, doi: 10.1016/S1359-835X(02)00259-2.
- [3] B. Rebba and N. Ramanaiah, "Evaluation of Mechanical Properties of Aluminium Alloy (Al-2024) Reinforced with Molybdenum Disulphide (MOS 2) Metal Matrix Composites," Procedia Materials Science, vol. 6, no. Icmpc, pp. 1161–1169, 2014, doi: 10.1016/j.mspro.2014.07.189.
- [4] "2024 Aluminium," p. 5273331, 1930.
- [5] H. Yang et al., "High-temperature mechanical properties of 2024 Al matrix nanocomposite reinforced by TiC network architecture," Materials Science and Engineering A, vol. 763, no. July, p. 138121, 2019, doi: 10.1016/j.msea.2019.138121.
- [6] M. Kok, "Production and mechanical properties of Al2O3 particle-reinforced 2024 aluminium alloy composites," Journal of Materials Processing Technology, vol. 161, no. 3, pp. 381–387, 2005, doi: 10.1016/j.jmatprotec.2004.07.068.
- [7] D. V. N, B. K. B, and G. K. M, "Microstructure, mechanical properties and fracture mechanisms of ZrB2 ceramic reinforced A7075 composites fabricated by stir casting," Materials Today Communications, vol. 25, no. May, p. 101289, 2020, doi: 10.1016/j.mtcomm.2020.101289.
- [8] P. S. Bains, S. S. Sidhu, and H. S. Payal, "Fabrication and Machining of Metal Matrix Composites: A Review," Materials and Manufacturing Processes, vol. 31, no. 5, pp. 553–573, 2016, doi: 10.1080/10426914.2015.1025976.
- [9] A. Albiter, C. A. León, R. A. L. Drew, and E. Bedolla, "Microstructure and heat-treatment response of Al-2024/TiC composites," Materials Science and Engineering A, vol. 289, no. 1, pp. 109–115, 2000, doi: 10.1016/S0921-5093(00)00900-X.
- [10] D. Steglich, W. Brocks, J. Heerens, and T. Pardoen, "Anisotropic ductile fracture of Al 2024 alloys," Engineering Fracture Mechanics, vol. 75, no. 12, pp. 3692–3706, 2008, doi: 10.1016/j.engfracmech.2007.04.008.
- [11] Z. H. Tan, B. J. Pang, B. Z. Gai, G. H. Wu, and B. Jia, "The dynamic mechanical response of SiC particulate reinforced 2024 aluminum matrix composites," Materials Letters, vol. 61, no. 23–24, pp. 4606–4609, 2007, doi: 10.1016/j.matlet.2007.02.069.
- [12] J. H. Shin, H. J. Choi, and D. H. Bae, "The structure and properties of 2024 aluminum composites reinforced with TiO2 nanoparticles," Materials Science and Engineering A, vol. 607, pp. 605–610, 2014, doi: 10.1016/j.msea.2014.04.038.

- [13] A. Shahsavari, F. Karimzadeh, A. Rezaeian, and H. Heydari, "Significant Increase in Tensile Strength and Hardness in 2024 Aluminum Alloy by Cryogenic Rolling," Procedia Materials Science, vol. 11, no. 2009, pp. 84–88, 2015, doi: 10.1016/j.mspro.2015.11.111.
- [14] H. S. Kumaraswamy, V. Bharat, and T. Krishna Rao, "Influence of Mechanical &tribological BehaviourOf Al 2024 MMC Fabricated by Stir Casting Technique-A Review," Materials Today: Proceedings, vol. 5, no. 5, pp. 11962–11970, 2018, doi: 10.1016/j.matpr.2018.02.170.
- [15] G. González-Doncel, S. D. Karmarkar, A. P. Divecha, and O. D. Sherby, "Influence of anisotropic distribution of whiskers on the superplastic behavior of aluminum in a back-extruded 6061 Al-20% SiCW composite," Composites Science and Technology, vol. 35, no. 2, pp. 105–120, 1989, doi: 10.1016/0266-3538(89)90091-2.
- [16] C. S. Ramesh, S. Pramod, and R. Keshavamurthy, "A study on microstructure and mechanical properties of Al 6061-TiB2 in-situ composites," Materials Science and Engineering A, vol. 528, no. 12, pp. 4125–4132, 2011, doi: 10.1016/j.msea.2011.02.024.
- [17] S. Yadav, D. R. Chichili, and K. T. Ramesh, "The mechanical response of a 6061-T6 A1/A12O3 metal matrix composite at high rates of deformation," Acta Metallurgica Et Materialia, vol. 43, no. 12, pp. 4453–4464, 1995, doi: 10.1016/0956-7151(95)00123-D.
- [18] N. K. Maurya, M. Maurya, A. K. Srivastava, S. P. Dwivedi, A. Kumar, and S. Chauhan, "Investigation of mechanical properties of Al 6061/SiC composite prepared through stir casting technique," Materials Today: Proceedings, vol. 25, no. xxxx, pp. 755–758, 2019, doi: 10.1016/j.matpr.2019.09.003.

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