

Mathematical Modeling and Analyzing of Piston Rings Used in Piston Cylinder attachment of the IC Engines

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ABSTRACT

This paper presents the piston ring sealing used in the piston cylinder attachment of the IC Engine. This developed model with the integrated model of gas and temperature in the arrangement as well as the displacement caused in the piston ring would be taken into account. Due to compression of the fuel, temperature may raises about 600 °C and pressure around 32 to 50 bar pressure so the thermal deformation takes place and wear of the piston ring occurs. Hence a mathematical model has been required for the safety operation of the piston ring and to obtain permissible limit range of working. This can be also implemented for the life time calculation. This paper describes about the assumptions made for obtaining the model as well as simulation of the obtained results in Solidworks as well as the Matlab Software.

KEYWORDS: *Mathematical model, Thermal deformation, displacement of rings, piston ring.*

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I. INTRODUCTION

Piston ring acts as a sealing device to minimize the leakage caused in the system. It should maintain high degree of contact with the surface of the cylinder. Simultaneously, it would act as a slider bearing due to sliding motion of the piston along the surface of the cylinder and also lubricated hydro-dynamically. Hence, it should have low coefficient of friction. Also, it should be ensured that it consumes minimum lubrication oil and runs for a long time [5, 13, 18 and 23].

On considering the gas flow type, the most cases it would be assumed as the aabyrinth sealing in which the gas may flow between the various stages by means of the gap between the rind and the cylinder. Various factors like pressure difference,

Viscosity and some other factors influence the flow of the gas. [1] He developed model that would satisfy the perfect gas laws and flow may be considered as isoentropic or adiabatic flow, when the fluid flows through an orifice.

Position of the rings and force exerted by it are the two major factors considered by most of the researchers. It decides the inner and behind ring spacing is connected. When the volume of the behind ring is greater than the inner ring, the accumulation action would takes place. In order to obtain the fine results they developed the integrated model of the gas flow along with the model of the axial displacement of the rings placed within the grooves [12, 8, 25, 9, 22 and 24]. In [19] the coefficient of the flow depends on the pressure ratio before and after the orifice. The approach of the mass flux determination was implemented in

the model [8, 9 and 20].

In most of the assumed adiabatic process, the flow would be assumed to be laminar and have low values of the Reynolds number usually less than 2000. The entire system may be assumed as the heat exchanger system (DOF = 3) where the exchange of the heat takes place between the gas and the surrounding walls [15, 19 and 20]. On considering the above factors [5,8] does not assume the process as an isothermal process. Some authors [6, 9, 13 and 21] had developed the model to obtain various thermal parameters such as adiabatic index, temperature, pressure and so on.

On this article, we had assumed the process as an adiabatic or isentropic process with laminar flow type so that the uniformity of the flow is obtained.

Reynolds Number < 2000

II. DESIGN OF GAS FLOW MODEL

Piston Model- Stress Analysis

Figure 1 and 2 shows the solid model of the piston along with the piston ring design developed by using the SolidWorks software. The various parts are designed individually and the entire model was assembled using the Solidworks.

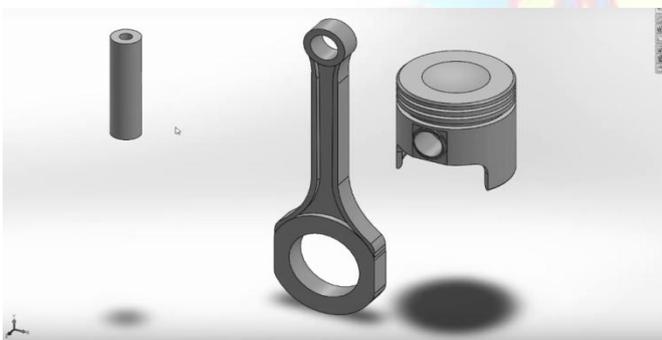


Figure 1 Part Model of the Piston

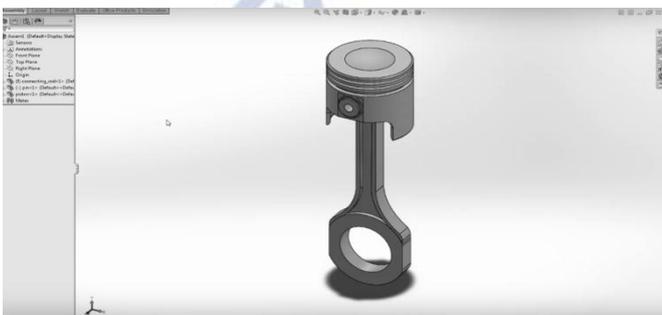


Figure 2 Assembled Model of the Piston

From the above mentioned figure, piston ring could be easily indentified. The above mentioned

assembly was subjected to stress analysis for which the parameters are selected as shown in the Figure 3 and the stress induced in the part are indentified in the Figure 4.

Property	Value	Units
Elastic Modulus	7.9e+010	N/m ²
Poissons Ratio	0.34	N/A
Shear Modulus	2.6e+010	N/m ²
Density	2680	kg/m ³
Tensile Strength	380000000	N/m ²
Compressive Strength in X		N/m ²
Yield Strength	315000000	N/m ²
Thermal Expansion Coefficient	1.94e-005	/K
Thermal Conductivity	138	W/(m.K)
Specific Heat	850	J/(kg.K)
Material Damping Ratio		N/A

Figure 3 Selected Parameters

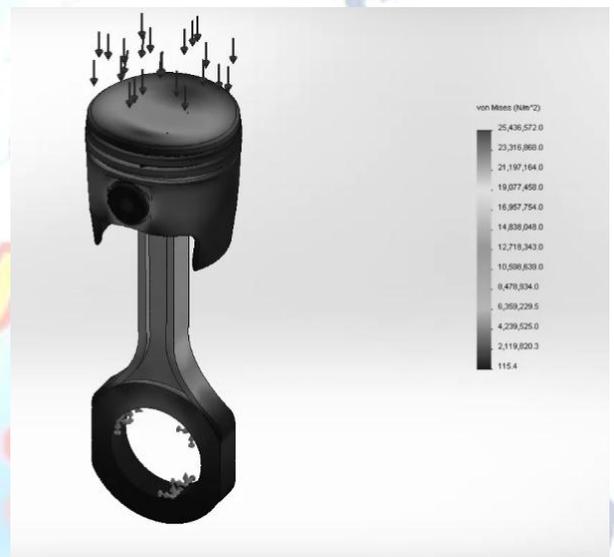


Figure 4 Stress Analysis

From the Figure 4 it should be noted that there would be more stress concentrated at the top of the piston arrangement that the stress concentration factor for the piston ring would be sufficiently more so that the design of the piston ring should be sufficient enough to withstand the stress and to capable for long life performance. Most of the load induced would be the distributed load.

Piston Ring Model – Force Analysis

Figure 5 shows the piston that can be used as the gas seal function in which the fluid flows from the top to bottom and the forces acting are resolved to three directions and they are:

- 1) Force along the X-axis on which the piston ring rests on.
- 2) Force along Y-axis which may be due to the fluid flow that would be restricted by the piston ring produces the downward movement.
- 3) Another force along Y-axis known as the reactive force that pushes and counter reacts the force which pushes the piston ring downwards.

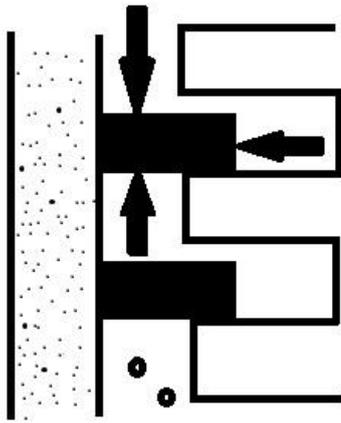


Figure 5 Gas Seal Function

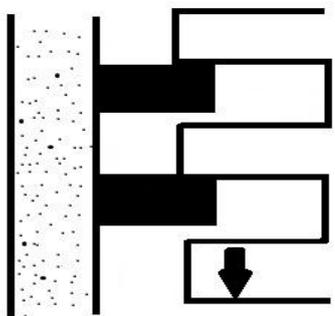


Figure 6 Gas Seal Function

Figure 6 denotes the movement of the piston ring from the bottom position to the top position after the gas flow takes place. As discussed the force analysis are shown in the Figure 7.

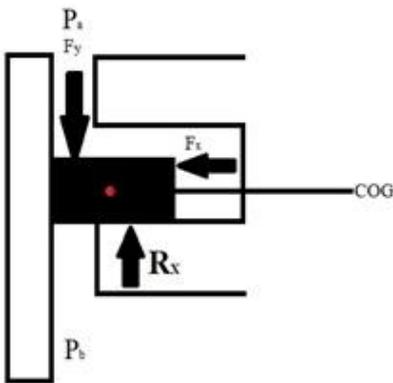


Figure 7 Force Analysis

In the Figure 7, F_x indicates the force along the X-axis, F_y indicates the force along Y-axis and R_x be the reactive force developed. Here, COG is the Center of the Gravity in which the whole mass of the piston ring arte said to be concentrated and it can be easily calculated by considering as the rectangular cross section.

Assume that there is no leakage of gases.

The Horizontal Forces may be given as,

$$F_x = 0$$

Vertical Forces can be resolved as,

$$F_y = -R_x$$

Summation of the horizontal and the vertical forces are assumed to be zero. So that the above mentioned equation becomes,

$$F_x + F_y = F_x - R_x$$

Therefore, it may be noted that the forces exerted due to the gas flow must be less than the reactive force developed by the piston ring in order to achieve the effective sealing performance.

Simscape Model

The Solidworks model has been converted into .xml file and it have been imported into the Matlab environment to obtain the simscape model for the so designed piston ring as shown in the Figure 8.

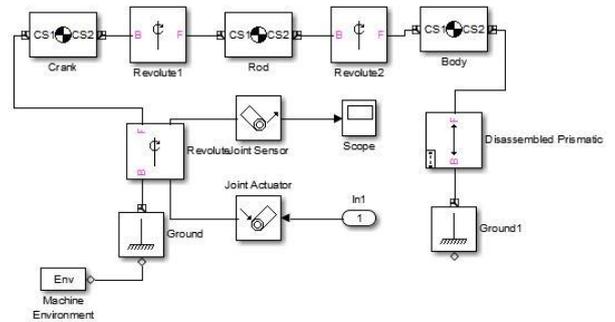


Figure 8 Simscape Model

III. CONCLUSION

From the analysis we could be able to find a conclusion that, for the Poisson ratio about 0.34 the value of the stress concentration factor is found to be minimum and hence the notch sensitivity reduces so the lifetime of the piston ring can be improved to a extent than in an ordinary condition. And the force should not exceed the yield point stress also the value of the thermal sensitivity should be low in order to have the low thermal stress.

REFERENCES

- [1] Keribar R., Dursunkaya Z., Flemming M.F.: An integrated model of ring pack performance. Trans ASME, Journal of Engineering for Gas Turbines and Power, Vol. 113, 1991, pp. 382-389.
- [2] Koszałka G.: Application of the piston-rings-cylinder kit model in the evaluation of operational changes in blowby flow rate. Eksploatacja i Niezawodność - Maintenance and Reliability Nr 4 (48)/2010, pp. 72-81.

- [3] Eweis M.: Reibungs und Undichtigkeitsverluste an Kolbenringen. Forschungshefte des Vereins Deutscher Ingenieure, 1935.
- [4] Aghdam E.A., Kabir M.M.: Validation of a blow-by model using experimental results in motoring condition with the change of compression ratio and engine speed. *Experimental Thermal and Fluid Science* 34 (2010), pp. 197–209.
- [5] Furuhashi S., Tada T.: On the flow of gas through the piston-rings, 2nd Report: the character of gas leakage. *Bull JSME* 1961; 4(16): pp. 691–698.
- [6] Iskra A.: Oil film parameters in the nodes of piston – crankshaft mechanism of combustion engine (in Polish). Publishing House of The Technical University of Poznań, (Wyd. Politechniki Poznańskiej) , Poznań, 2001.
- [7] Namazian M., Heywood J.B.: Flow in the piston-cylinder-ring crevices of a spark-ignition engine: effect on hydrocarbon emissions, efficiency and power. SAE Paper 820088, 1982.
- [8] Mufti R.A., Priest M., Chittenden R.J.: Analysis of piston assembly friction using the indicated mean effective pressure experimental method to validate mathematical models. *Proc. Instn Mech. Engrs, Part D: Journal of Automobile Engineering*, 222(8): pp.1441-1457, 2008.
- [9] Miyachika M., Hirota T., Kashiyama K.: A consideration on piston second land pressure and oil consumption of internal combustion engine. SAE Paper 840099, 1985.
- [10] Petris De C., Giglio V., Police G.: A mathematical model for the calculation of blow-by flow and oil consumption depending on ring pack dynamics, Part I: gas flows, oil scraping and ring pack dynamics. SAE Paper 941940, 1994
- [11] Rakopoulos C.D., Kosmadakis G.M., Dimaratos A.M., Parotis E.G.: Investigating the effect of crevice flow on internal combustion engines using a new simple crevice model implemented in a CFD code. *Applied Energy* 88 (2011), pp. 111–126.
- [12] Serdecki W.: Research on interaction of elements of piston-cylinder system in combustion engine (in Polish). Publishing House of The Technical University of Poznań, (Wyd. Politechniki Poznańskiej) , Poznań 2002.
- [13] Tian T., Noordzij L.B., Wong V.W., Heywood J.B.: Modeling piston-ring dynamics, blowby and ring-twist effects. *Trans ASME, Journal of Engineering for Gas Turbines and Power*, Vol. 120, No 4, 1998, pp. 843-854.
- [14] Koszałka G.: Modelling the blowby in internal combustion engine, Part 1: A mathematical model. *The Archive of Mechanical Engineering*, Vol. LI (2004), No. 2, pp. 245-257.
- [15] Koszałka G.: Application of the piston-rings-cylinder kit model in the evaluation of operational changes in blowby flow rate. *Eksplatacja i Niezawodność - Maintenance and Reliability* Nr 4 (48)/2010, pp. 72-81.
- [16] Kuo T-W., Sellnau M.C., Theobald M.A., Jones J.D.: Calculation of flow in the piston-cylinder-ring crevices of a homogeneous-charge engine and comparison with experiment. SAE Paper 890838, 1989.
- [17] Merkisz J., Tomaszewski F., Ignatow O.: Service life and diagnostics of piston node in combustion engines (in Polish). Publishing House of The Technical University of Poznań, (Wyd. Politechniki Poznańskiej), Poznań, 1995
- [18] Wannatong K., Chanchaona S., Sanitjai S.: Simulation algorithm for piston ring dynamics. *Simulation Modelling Practice and Theory* 16 (2008) 127–146.
- [19] Wolff A.: Numerical analysis of piston ring pack operation. *Combustion Engines* 2/2009 (137), pp. 128141
- [20] Yoshida H., Yamada M., Kobayashi H.: Diesel engine oil consumption depending on piston ring motion and design. SAE Paper 930995, 1993.
- [21] Niewczas A.: Service life of piston-rings-cylinder unit in combustion engine (in Polish) . WNT , Warszawa, 1998.
- [22] Munro R.: Blow-by in relation to piston and ring features. SAE Paper 810932, 1982.
- [23] Miyachika M., Hirota T., Kashiyama K.: A consideration on piston second land pressure and oil consumption of internal combustion engine. SAE Paper 840099, 1985.
- [24] Mufti R.A., Priest M., Chittenden R.J.: Analysis of piston assembly friction using the indicated mean effective pressure experimental method to validate mathematical models. *Proc. Instn Mech. Engrs, Part D: Journal of Automobile Engineering*, 222(8): pp.1441-1457, 2008.
- [25] Furuhashi S., Tada T.: On the flow of gas through the piston-rings, 1st Report: the discharge coefficient and temperature of leakage gas. *Bull JSME* 1961; 4(16): pp. 684–690.
- [26] Ye X M. Numerical investigation and application of threedimensional lubrication performance in piston ring pack. (In Chinese). PhD Thesis, Huazhong University of Science and Technology, China, 2004.
- [27] Elsharkawy A A, Alyaout S F. Optimum shape design for surface of a porous slider bearing lubricated with couple stress fluid. *Lubr Sci* 21(1): 1–12 (2009)
- [28] Skopp A, Kelling N, Woydt M, Berger L M. Thermally sprayed titanium suboxide coatings for piston ring/cylinder liners under mixed lubrication and dry-running conditions. *Wear* 262(9–10): 1061–1070 (2007)
- [29] Wong V W, Tung S. Overview of automotive engine friction and reduction trends-Effects of surface, material and lubricant-additive technologies. *Friction* 4(1): 1–28 (2016)
- [30] Styles G, Rahmani R, Rahnejat H, Fitzsimons B. In-cycle and life-time friction transience in piston ring–liner conjunction under mixed regime of lubrication. *Int J Eng Res* 15(7): 862–876 (2014)